A sheath model for arbitrary radiofrequency waveforms

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RF Plasmas in industry

Frequency domain

Figure 4.1 A capacitively coupled electrode adjacent to a plasma excited by some unspecified external means; $V = V_1 \sin \omega t$.

Traditional capacitive discharges

Impedance depends on :

- Voltage, V_{rf}
- Electron density, n_e
- Sheath size, s_m

To find a self-consistent solution:

- Child law
- Particle balance
- Power balance

Dual Frequency with well separated frequencies

A. Perret et al., Appl. Phys. Lett 86 (2005) 021501

Dual Frequency Capacitive (DFC)

Electrical assymmetry effect

• It is possible to change the self-bias by changing the phase between the two frequencies, even when geometrically symmetrical

- The asymmetry is generated by the voltage waveform
- B. G Heil, U. Czarnetzki, RP Brinkmann and T.Mussenbrock, J. Phys. D: Appl. Phys. **41** (2008) 165202

Complex waveforms

Number of Harmonics

- Electron heating is also affected
- T. Lafleur, P.A. Delattre, E.V. Johnson, and J.P. Booth, Appl. Phys. Lett. (2012)

Motivation

- The sheath is the most important element in capacitive discharges
- Electron heating, EEDF, IEDF on the substrate are all determined by the sheath physics
- Lieberman (after Godyak) supplied an analytical model of the RF sheath for sinusoidal waveform [IEEE Trans. Plasma Sci. 16, 638 (1988)]
- Lieberman's model cannot be generalized to arbitrary RF waveforms
- In this talk we present an analytical model for arbitrary RF waveforms

The DC sheath

The DC sheath

• The Child-Langmuir law

The « real » RF sheath

RF sheaths models

Single frequency, sine wave:

• Valery Godyak, "Soviet Radiofrequency Discharge Research", Delphic Associates, Fall Church, 1986 • Michael Lieberman, IEEE Plasma Sci. **16** (1988) 638

Dual frequency, sine wave:

• Jérôme Robiche, P C Boyle, M M Turner and A R Ellingboe, J. Phys. D. **36** (2003) 1810

More recently (including kiinetic effects and arbitrary waveforms):

- Brian G Heil et al J. Phys. D: Appl. Phys. **41** (2008) 225208
- Mohammed Shihab et al J. Phys. D: Appl. Phys. **45** (2012) 185202
- Uwe Czarnetzki , Physical Review E **88,** 063101 (2013)
- Miles Turner and Pascal Chabert, Appl. Phys. Lett. **104**, 164102 (2014)
- P Chabert and M M Turner, J. Phys. D : Appl. Phys. **50** (2017) 23LT02

The trick

Time-averaged quantities

$$
J_i = K_i \frac{\epsilon_0}{s_m^2} \left(\frac{2e}{M}\right)^{\frac{1}{2}} \left(-\bar{V}\right)^{\frac{3}{2}}
$$

$$
n_i(x) = -\frac{4}{9} \frac{\epsilon_0 \bar{V}}{\xi e s_m^2} \left(\frac{s_m}{x}\right)^{\frac{2}{3}}
$$

$$
\bar{\phi}(x) = \bar{V} \left(\frac{x}{s_m}\right)^{\frac{4}{3}}
$$

$$
\bar{E}(x) = -\frac{4}{3} \frac{\bar{V}}{s_m} \left(\frac{x}{s_m}\right)^{\frac{1}{3}}
$$

 n/n_0

Time-dependent quantities

Find ξ

$$
\frac{\bar{V}}{V_0} = \frac{\bar{\rho}}{\rho_0} \equiv \xi \qquad V(t) = V_0 \left[1 - \frac{4}{3} \left(\frac{s}{s_m} \right)^{\frac{1}{3}} + \frac{1}{3} \left(\frac{s}{s_m} \right)^{\frac{4}{3}} \right]
$$
\n
$$
\xi = \frac{\langle V(t) \rangle}{V_0} = \left\langle 1 - \frac{4}{3} \left(\frac{s}{s_m} \right)^{\frac{1}{3}} + \frac{1}{3} \left(\frac{s}{s_m} \right)^{\frac{4}{3}} \right\rangle
$$

The procedure

• Current waveform as the input parameter

• Find s(t):
$$
J = \epsilon_0 \left. \frac{\partial E}{\partial t} \right|_{x=s_m} = \frac{4}{3} \frac{\epsilon_0 V_0}{s_m} \frac{d}{dt} \left(\frac{s}{s_m} \right)^{\frac{1}{3}} \qquad \frac{s}{s_m} = \left[\frac{3}{4} \frac{s_m}{\epsilon_0 V_0} \int_0^t J dt \right]^3
$$

• Find ξ and $V(t)$: $\xi = \frac{\langle V(t) \rangle}{V_0} = \left\langle 1 - \frac{4}{3} \left(\frac{s}{s_m} \right)^{\frac{1}{3}} + \frac{1}{3} \left(\frac{s}{s_m} \right)^{\frac{4}{3}} \right\rangle$

$$
V(t) = V_0 \left[1 - \frac{4}{3} \left(\frac{s}{s_m} \right)^{\frac{1}{3}} + \frac{1}{3} \left(\frac{s}{s_m} \right)^{\frac{4}{3}} \right]
$$

• All other parameters are then easily calculated

Example 1: sine wave

For the single frequency case treated by Lieberman [9] we choose $J(t) = -J_0 \sin \omega t$. From Eqs. (15) and (14) we find

$$
s(t) = \frac{s_m}{8} \left(1 - \cos \omega t \right)^3 \tag{16}
$$

$$
J_0 = -\frac{K_{\rm cap}}{2} \frac{\omega \epsilon_0}{s_m} V_0 \tag{17}
$$

$$
\xi = \frac{163}{384} \tag{18}
$$

where $K_{\text{cap}} = 4/3$. The voltage waveform is obtained by inserting Eq. (16) into Eq. (12). Combining Eqs. (5) and (17) gives the sheath maximum expansion as a function of J_0 ,

$$
s_m = \frac{K_s J_0^3}{e\epsilon_0 k_B T_0 \omega^3 n_0^2},\tag{19}
$$

where $K_s = 4\xi/3$. These expressions are identical with those of Lieberman [1, 9], apart

Example 1: sine wave

Example 2: pulsed waveform

As a third example we consider a sheath excited by the pulsed waveform

$$
J(t) = J_0 \left(\frac{t}{t_w}\right) \exp\left(\frac{1}{2} - \frac{1}{2} \frac{t^2}{t_w^2}\right),\tag{26}
$$

which is representative of several topical experiments $[10-12]$. We assume that this pulse is repeated at intervals $t_p \ll t_w$, such that successive pulses do not appreciably overlap. In this case we find

$$
s(t) = s_m \exp\left(-\frac{3}{2}\frac{t^2}{t_w^2}\right) \tag{27}
$$

$$
\xi = 1 - \frac{7}{3} \sqrt{\frac{\pi}{2}} \frac{t_w}{t_p} \tag{28}
$$

$$
J_0 = -\frac{4}{3} \frac{\epsilon_0 V_0}{s_m t_w \exp\left(\frac{1}{2}\right)}\tag{29}
$$

$$
s_m = \frac{\xi}{6} \exp\left(\frac{3}{2}\right) \frac{\left(J_0 t_w\right)^3}{\epsilon_0 e n_0^2 k_B T_0} \tag{30}
$$

Example 2: pulsed waveform

Conclusions

- A sheath model has been developed for arbitrary RF waveforms
- Agrees well with PIC simulations
- Can be extended to two sheaths and then calculate bias formation (see Electrical Assymetry Effect Bochum)
- Heating in the sheath (both collisionless and ohmic) can be calculated analytically: therefore a global model can easily be constructed

The full CCP with arbitrary waveform

Theory for the self-bias formation in capacitively coupled plasmas excited by arbitrary waveforms T Lafleur, P Chabert, M M Turner and J P Booth Plasma Sources Sci. Technol. **22** 065013 (2013)

$$
\frac{s_R}{s_{mR}} = \alpha_R \left[\frac{\int_{t_0}^t I dt}{\int_{t_0}^{t_m} I dt} \right]^3
$$

$$
\frac{s_L}{s_{mL}} = 1 - (1 - \alpha_L) \left[1 - \frac{\int_{t_0}^t I dt}{\int_{t_0}^{t_m} I dt} \right]^3
$$

- 2

 $S_1 = 0$

$$
\frac{V_R}{V_{0R}} = \left[1 - \frac{4}{3} \left(\frac{s_R}{s_{mR}}\right)^{1/3} + \frac{1}{3} \left(\frac{s_R}{s_{mR}}\right)^{4/3}\right]
$$

$$
\frac{V_L}{V_{0L}} = \left[1 - \frac{4}{3} \left(\frac{s_{mL} - s_L}{s_{mL}}\right)^{1/3} + \frac{1}{3} \left(\frac{s_{mL} - s_L}{s_{mL}}\right)^{4/3}\right]
$$

Self-bias

$$
\eta = \frac{1}{T} \int_0^T V_{rf} dt = \frac{1}{T} \int_0^T (V_L - V_R) dt = \xi_L V_{0L} - \xi_R V_{0R}
$$

- Dashed line is when conduction current balance is not satisfied
- Excellent agreement with PIC results if conduction current balance is satisfied (blue line)

$$
n_0 u_B = \frac{1}{T} \int_0^T \frac{1}{4} n_0 \bar{v}_e e^{V_R/T_e} dt
$$

$$
n_0 u_B = \frac{1}{T} \int_0^T \frac{1}{4} n_0 \bar{v}_e e^{V_L/T_e} dt
$$

Plasma potential

• Plasma potential waveform can be obtained analytically

$$
V_p = -V_R
$$

$$
V_{rf} = V_L + V_p = V_L - V_R
$$

• Excellent agreement with PIC results

