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Gaine et modélisation fluide du plasma de bord en fusion magnétique: besoins, questions ouvertes...

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The heat exhaust issue in a nutshell

- In magnetic fusion devices (e.g. tokamaks), a large amount of power is convected by the plasma to the wall of the machine
- Anisotropy of magnetized plasma => power deposited on very thin layer on the wall
- E.g., in ITER: unacceptable heat loads!

 $50 MW \quad 100 MW \quad 50 MW$ $= P_{heat} + 0.2 P_{fus} - P_{rad} \approx 100 MW$ $P_{wall} = \frac{P_{plasma}}{4\pi R f_{geo} \lambda_q} \sim 130 MW \cdot m^{-2} \gg P_{max}$ $6 m \sim 10 \sim 1 mm$





Plasma neutral interactions in the divertor

- Divertor recycling: ions impact wall re-enter the plasma after recombining at the wall
 - on metallic surfaces, $\mathbf{R}_n \approx 100\%$
 - re-enter as atoms or molecules
- Zoo of plasma-neutrals interactions
 - Transfer of plasma momentum and energy to non-confined particles





Detachment as a heat exhaust strategy

• 2-point model: $\Gamma_t = \left(\frac{n_u^2}{q_{\parallel}}\right) \left(\frac{7}{2} \frac{q_{\parallel}L}{\kappa_{0e}}\right)^{4/7} \frac{\gamma e^2}{2m_i}$

[Stangeby, The Plasma Boundary of Magnetic Fusion Devices]

- At least 20eV lost per recycling particle => drop of temperature and heat flux
- Can be amplified by seeding mid-heavy impurities (e.g., N or Ne)





- High enough density \Rightarrow plasma momentum and energy entirely transferred to photons and neutrals
 - Below 1eV: recombination before the wall => detachment

Detachment in practise

In experiments:







In numerical modelling (SOLEDGE3X applied to ITER):



Fluid edge plasma codes as the work-horse

Impurities

Wall

- Key question: can one reach detachment without impacting negatively discharge performance and stability?
 - Design of divertor and sub-systems

Fluid!

 Determine operational space: fuelling, upstream density, impurity seeding...

Plasma

(turbulent)

transport

Extremely non-linear & multi-physics system



SOLEDGE3X: a versatile fluid code for the edge plasma

- SOLEDGE3X: multi-fluid modelling tool for the edge plasma resulting from merge of SOLEDGE2D (2D transport code like SOLPS) and TOKAM3X (3D turbulence code)
- Key features:
 - Neutrals either fluid (embedded) or kinetic (EIRENE)
 - Arbitrary plasma composition based on Zhdanov closure
 - Complete plasma geometrical flexibility (arbitrary number of Xpoints)
 - Simulations up-to-the first wall with full wall geometry
 - Usable in 2D or 3D
 - Usable as mean-field or self-consistent turbulence code

	Mean-field	Turbulence
2D	\checkmark	\checkmark
3D	\checkmark	\checkmark

More information and references on www.soledge3x.com









3D turbulence

And the sheath in all this?

- Sheath physics enters the modelling at 2 places:
 - Boundary condition for the plasma fluid code
 - Typically at magnetic pre-sheath entrance
 - Position assumed to be the same as the wall in spite of extremely short mean-free path for molecules
 - Boundary conditions for kinetic neutrals
 - Emitted from the wall
 - Implicit sheath model to determine link with local plasma properties (flux, density, temperature, composition...)



Plasma fluid:

- fluxes (particle, momentum, energy)?
- Electrostatic and magnetic potential?



Kinetic neutrals:

- Energy and angular distribution function?
- Chemical nature?

Sheath boundary conditions in SOLEDGE3X

- Edge plasma fluid codes all rely on some flavor of Bohm boundary conditions
- In SOLEDGE3X, Bohm-Chodura for oblique incidence with drifts and single ion species

 $\begin{aligned} u_{\parallel i} \vec{b} \cdot \vec{n} &\geq c_s \vec{b} \cdot \vec{n} - \vec{u}_{\perp i} \cdot \vec{n} \\ \vec{j} \cdot \vec{n} &= \vec{\Gamma}_{n_i} \cdot \vec{n} \left(1 - e^{\Lambda - \frac{e\Phi}{T_e}} \right) \\ \vec{\Gamma}_{E_{e/i}} \cdot \vec{n} &= \gamma_{e/i} T_{e/i} \vec{\Gamma}_{n_{e/i}} \cdot \vec{n} \end{aligned}$

$$c_{s} = \sqrt{\frac{Z_{i}T_{e} + T_{i}}{m_{i}}}$$

$$\Lambda = -0.5 \ln\left(2\pi \frac{m_{e}}{m_{i}}\left(1 + \frac{T_{i}}{T_{e}}\right)\right)$$

 \vec{B}

Typically $\gamma_i = 2.5$ and $\gamma_e \approx 4$

Alternate fluid boundary conditions exist but similar

Loizu et al. proposed alternate sheath boundary conditions for fluid codes [Loizu, PoP 2012]





- Overall similar to Bohm-Chodurah with additional correction terms
 - Boundary condition on T_e raises questions concerning heat fluxes

So what is the issue?

- Issue: relevant reactor plasma conditions are not compatible with collison-less sheath for simple plasma at large incidence angle
 - Sheath heat transmission factors and fluid plasma description
 - Large range of collisionalities from collision-less to diffusive sheath
 - Complex plasma mix with possibly several dominant ion species
 - E.g., ITER high power seeded plasma: D + T + He + Ne + W
 - Small incidence angles are ubiquitous



	Low v_{col}	High v_{col}
Single ion	Bohm	
Trace imp.		
Arbitrary		

Sheath heat transmission factors

Sheath heath transmission factors = kinetic correction to fluid model

> $\vec{\Gamma}_{\mathrm{E}_{e/i}} \cdot \vec{n} = \gamma_{e/i} T_{e/i} \vec{\Gamma}_{\mathrm{n}_{e/i}} \cdot \vec{n}$ Typically $\gamma_i = 2.5$ and $\gamma_e \approx 4$

- Small fraction of hot electrons enough to deviate strongly from classical values
 - Very dependent on plasma conditions
 - Can be problematic even at high collisionality (example here)



Friction with neutrals pushes away from Bohm (1)

BIT1 (1D/3V kinetic SOL) simulations at high density
 *M*_{||} < 1 everywhere due to friction with neutrals

If SE = last point where plasma still magnetized

 $M_{\parallel} = M_{\chi} / \sin \theta$

• Correction to Bohm:

.

$$\chi = \frac{(\nu_{mt}(1-\alpha) + \nu_{ei})x_0}{2c_s \sin \theta} \qquad \alpha = \frac{u_{\parallel n}}{u_{\parallel i}}$$

 $M_{\parallel} = 1 + \chi - \sqrt{\chi^2 + 2\chi}$

$$M_{\perp}(x_0) = \sin\theta \sim 20\rho_i$$





Consequences:

05/11/2024

[Tskhakaya, TSVV3 internal meeting]

Arbitrary

 $n_{\Gamma_i=const} / n_0$

10⁰

High v_{col}

Tskhakaya

14

Wall density increases • Heat flux to the wall decreases in spite of γ_e \nearrow Application to ITER low power case: SOL ring at max. outer target load

80 u₁₁, M₁₁=1 u,, M,=0.6 60 (kms⁻¹) 40 20 0 -20 50 100 150 0 parallel distance from inner target (m)

• Potential drop: $\frac{e\Delta\Phi}{T_e} = \Lambda T_e - 0.5 \ln M_{\parallel}$



150

100

parallel distance from inner target (m)

10

Friction with neutrals pushes away from Bohm (2)

5

4

3

1

0

0

50

 $(10^{20} m^{-3})$

Single dominant species at high collisionality

Multi-species BIT1 (1D/3V kinetic SOL) simulations at high density with 1 dominant species (D)





SE

Strong coupling between main and impurity ions

$$M_{\parallel i} = M_{\parallel}^{main} \sqrt{\frac{m_i}{m_{main}}}$$

$$M_{\parallel}^{main} = 1 + \chi - \sqrt{\chi^2 + 2\chi}$$

[Tskhakaya, TSVV3 internal meeting]

	Low v_{col}	High v_{col}
Single ion	Bohm	Tskhakaya 1
Trace imp.	?	Tskhakaya 2
Arbitrary		

—D⁺ —Ar⁺

-Ar++

—Ar⁺³

-Ar+4

10⁻²

Arbitrary mix: no clear solution at low-medium v_{col}

Initial kinetic simulations with multi-dominant species => no D-T coupling!



[Tskhakaya, TSVV3 internal meeting]

	Low v_{col}	High v_{col}
Single ion	Bohm	Tskhakaya 1
Trace imp.	?	Tskhakaya 2
Arbitrary	?	

Arbitrary mix: a guess for high v_{col} (1)

- Haven't heard (▲ not expert!) of sheath BC for fluid models with arbitrary ion mix
 - Here attempt at guessing a back-of-the-envelop behavior
- Reasonable assumption: high $v_{col} \Rightarrow \forall i, j \ u_{\parallel i} = u_{\parallel j} = u_{\parallel j}$



$$\partial_t N + \partial_z (N u_{\parallel}) = S_N$$

$$M \partial_t (N u) + M \partial_z (N u_{\parallel}^2)$$

$$= -\partial_z (NT) + Z e N E_{\parallel} + R_{\parallel} + S_p$$

$$n_e = ZN$$

$$0 = -\partial_z (n_e T_e) - e n_e E_{\parallel} + R_{\parallel e} + S_{p_e}$$

$$R_{\parallel} + R_{\parallel e} = 0$$

Equivalent single ion species plasma

$N = \Sigma_i n_i$	$MN = \Sigma_i m_i n_i$
$ZN = \Sigma_i Z_i n_i$	$NT = \Sigma_i n_i T_i$

05/11/2024

Arbitrary mix: a guess for high v_{col} (2)

Single-ion-species plasma equivalent to arbitrary ion mix:

 $N = \Sigma_i n_i \qquad MN = \Sigma_i m_i n_i$ $ZN = \Sigma_i Z_i n_i \qquad NT = \Sigma_i n_i T_i$

Then apply standard Bohm / Bohm-Chodurah / Tskhakaya:

$$\begin{split} \Delta \Phi &\equiv \Lambda T_{\rm e} = -0.5 T_e \ln \left(2\pi \frac{m_e}{M} \left(Z + \frac{T}{T_e} \right) \right) \\ u_{\parallel} &\geq \sqrt{\frac{Z T_e + T}{M}} \\ \gamma_i &= 2.5 \\ \gamma_e &= 2 + \frac{e \Phi}{T_e} \end{split}$$

	Low v_{col}	High $ u_{col}$
Single ion	Bohm	Tskhakaya 1
Trace imp.	?	Tskhakaya 2
Arbitrary	?	Mean spec.?



The problem of grazing angles

Parallel incidence BIT1 simulations without drifts show

expected reverse sheath [Tskhakaya, TSVV3 internal meeting]

Not clear down to which angle this is valid

 $u_{\parallel i}\vec{b}\cdot\vec{n} \ge c_s\vec{b}\cdot\vec{n} - \vec{u}_{\perp i}\cdot\vec{n} \quad \Rightarrow \quad u_{\parallel i} = c_s$

Incidence angle along ITER wall



15^x 10⁵ 10 Electric field EI. 10^{18′} ج لال 10 D^+ 10¹ Density 10¹⁶ 10⁻⁶ 10⁻⁴ 10⁻⁵ 10⁻³ 10⁻² 10⁻⁶ 10⁻⁵ 10⁻³ 10^{-1} 10^{-4} 10^{-2} 10^{-1} x [m] x [m]

Which drift velocity?

- Bohm-Chodura and Loizu boundary conditions depend on drift-velocities
 - Both derived for cold ions, considering only ExB drift
 - At low incidence, drift term is not just a minor correction

$$u_{\parallel i} = c_s \left(\frac{\vec{u}_{\perp i} \cdot \vec{n}}{\vec{b} \cdot \vec{n}} \right)$$
 dominant if $\tan \alpha < \frac{|\vec{u}_{\perp i}|}{c_s}$

- But fluid-drift theory involves 2 first order drifts: ExB and diamagnetic
 - Should one retain the diamagnetic drift even though it does not transport gyrocenters? What about additional drifts due to friction with neutrals?



EADF at the wall matters (1)

- Energy recycling coefficient sensitive to angle of incidence
 - probability of fast specular reflection vs thermalization
 - Energy and Angular Distribution Function (EADF) at the solid surface matters

[Bufferand, J. Nucl. Mater. 2015]

- Standard sheath model (shifted Maxwellian) over-simplified and does not account for gyro-motion
 - Use PIC code database instead







EADF at the wall matters (2)

- PIC database results in very different incidence angle
 - Mainly due to gyro-motion
- Changing the sheath model can significantly change plasma solution [Marandet, PSI conf. 2018]



 Results currently being revisited and extended at LAPLACE laboratory within ANR PLATUN





Conclusion

- Sheath is not explicitly modelled in edge plasma codes because of lengths and time scales
 - Appear as boundary conditions or 0D implicit models
- The choice of the sheath model heavily influences results as it determines all fluxes to the wall
- Here browsed many issues related to limits of available sheath models:
 - Consistency between fluid (pre-sheath) and kinetic (sheath) models
 - Sheath for arbitrary plasma mix
 - Large range of collisionalities, especially large collisionality
 - Low incidence angles making perpendicular motion important (gyro-motion and/or drifts)
 - others exist, e.g. inclusion of secondary electron
- Current state of the art: pieces of solutions for each sub-issue, but no model covering all the needs